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**Butsch**

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(54) **BIPOLAR FORCEPS**

(56) **References Cited**

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(DE)

U.S. PATENT DOCUMENTS

(\*) Notice: Subject to any disclaimer, the term of this  
patent is extended or adjusted under 35  
U.S.C. 154(b) by 1228 days.

3,685,518 A	8/1972	Beuerle et al.	
6,293,946 B1 *	9/2001	Thorne	606/48
2006/0276785 A1 *	12/2006	Asahara et al.	606/51
2007/0265619 A1 *	11/2007	Ariola et al.	606/51
2008/0200914 A1 *	8/2008	Hanlon et al.	606/48

(21) Appl. No.: **13/171,575**

FOREIGN PATENT DOCUMENTS

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DE	60027311	1/2007
DE	102008022889 A1	6/2009
WO	WO01/15615	3/2001
WO	WO2006/103671	10/2006

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\* cited by examiner

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(51) **Int. Cl.**

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**B25B 9/02** (2006.01)

**A61B 17/30** (2006.01)

**A61B 18/14** (2006.01)

(52) **U.S. Cl.**

CPC . **B25B 9/02** (2013.01); **A61B 17/30** (2013.01);  
**A61B 18/1442** (2013.01); **A61B 2018/1462**  
(2013.01); **Y10T 29/49117** (2015.01)

(58) **Field of Classification Search**

CPC ..... **A61B 17/30**; **A61B 18/1442**; **A61B**  
**2018/1462**; **B25B 9/02**

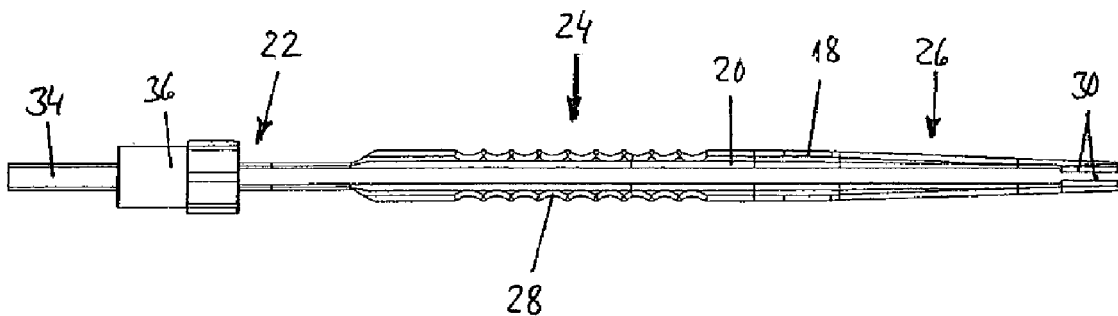
USPC ..... 606/45–52

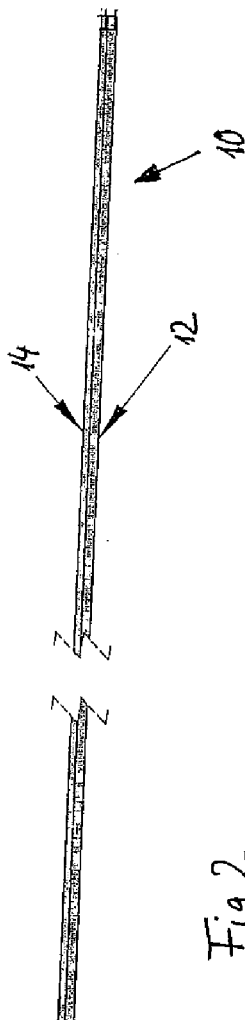
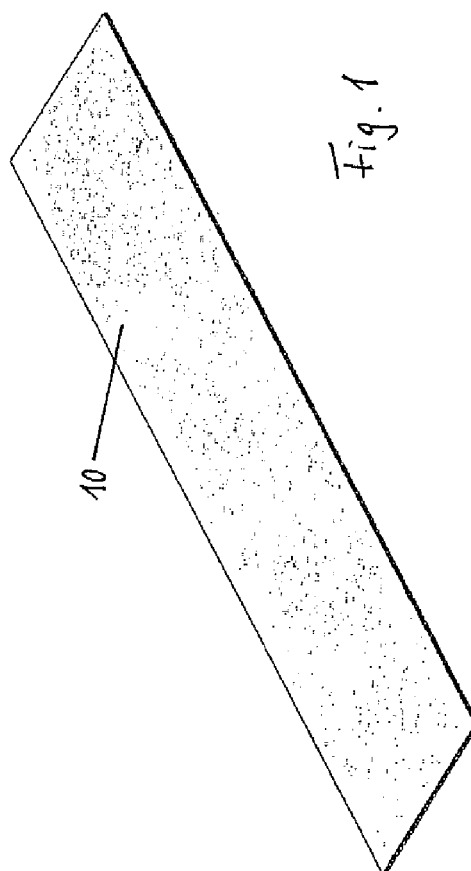
See application file for complete search history.

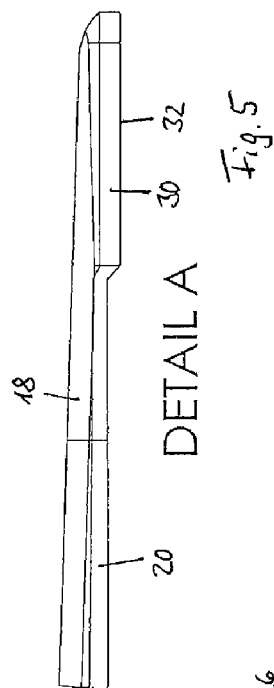
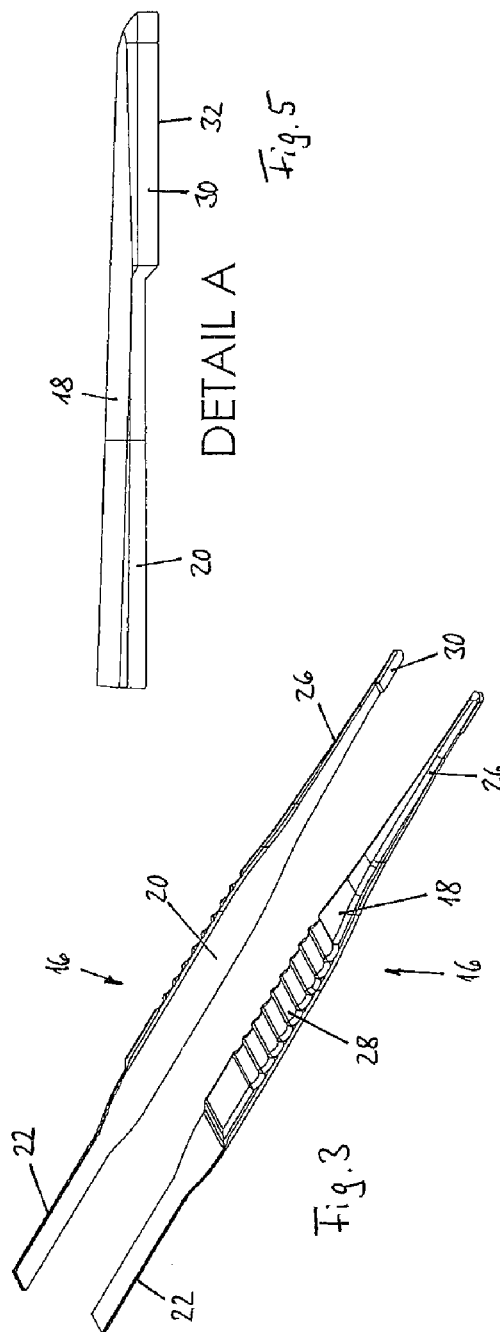
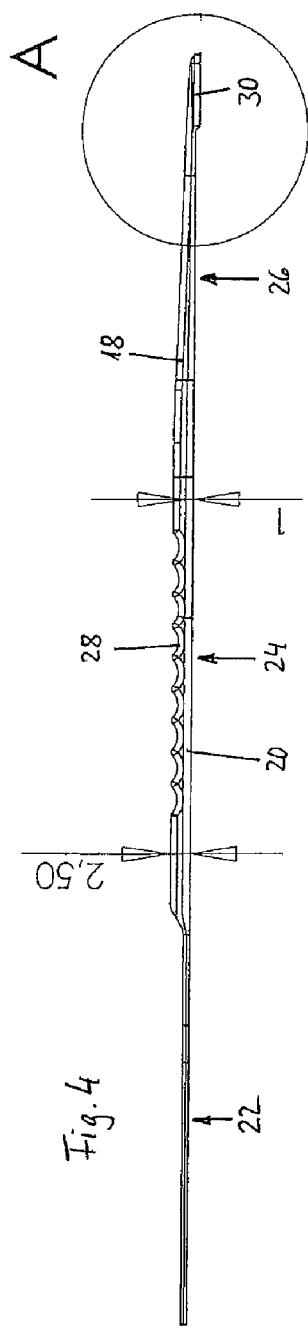
(57) **ABSTRACT**

The limbs of a bipolar forceps for RF coagulation are produced from a bimetal material, wherein an outer layer (18) consists of stainless steel and determines the mechanical properties of the forceps, while an inner layer (20) consists of a sliver alloy. An electrode (30) is formed from the inner layer at the distal end of the limbs (16). The inner layer (20) brings about good heat dissipation from the electrodes (30) and prevents the tissue from sticking thereto during coagulation.

**10 Claims, 3 Drawing Sheets**







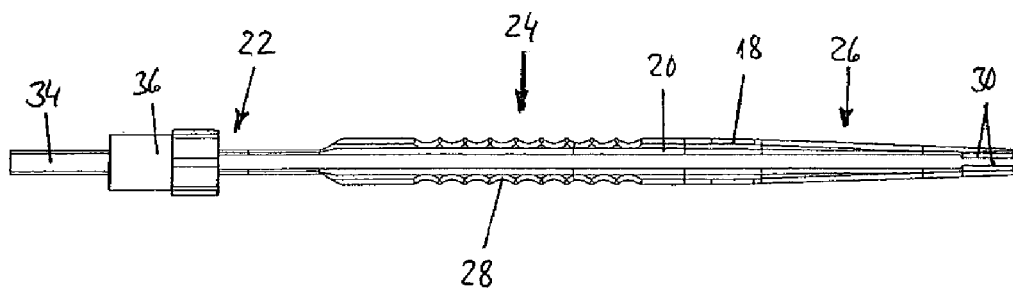
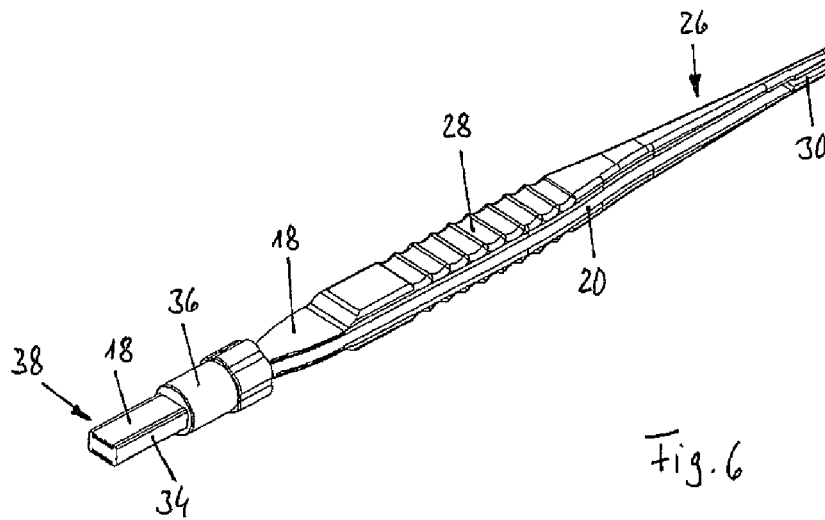


Fig. 7

# 1

## BIPOLAR FORCEPS

### BACKGROUND OF THE INVENTION

The invention relates to a bipolar forceps, more particularly for RF coagulation, as per the preamble of patent claim 1.

In surgery, bipolar forceps are used for coagulating the tissue of a patient. To this end, radiofrequency AC current is generally conducted through the tissue in order to heat and coagulate the latter. The forceps used for this purpose have differently shaped limbs, depending on intended use, with respectively one electrode being formed at the distal tips of the two limbs. The tissue to be coagulated is brought between the electrodes. The RF current is supplied via a plug-in connector attached proximally on the forceps and conducted through tissue via the electrodes.

A problem in the case of these bipolar forceps is that the RF current heats not only the tissue situated between the electrodes. The electrical contact resistance between the tissue and the contact areas of the electrodes touching the tissue also leads to heating of the electrodes. The heating of the electrodes can lead to the tissue sticking to the contact area of the electrodes. This leads to dirtying of the contact areas by the stuck-on tissue and increases the contact resistance for subsequent coagulations. Moreover, the tissue sticking-on can lead to stuck-on tissue parts being carried along when the forceps is removed and the tissue being damaged as a result of this.

In order to counteract this sticking-on of the tissue, the heating of the electrodes is known to be reduced by providing the electrodes with a metal, which has a high thermal conductivity for dissipating heat from the contact area of the electrodes. Moreover, this metal must have good electrical conductivity in order to conduct the RF current. Finally, the metal must be biocompatible, i.e. it must not damage the tissue chemically. Suitable metals with these properties are, in particular, the precious metals silver and gold, wherein silver should be preferred, more particularly also for reasons of cost. In the case of a bipolar forceps known from EP 1 210 022 B1, the distal tips of the limbs, consisting of stainless steel, of the forceps are for this purpose surrounded by a layer of silver or gold. This layer forms the electrodes with the contact areas thereof and at the same time forms a heat reservoir with a relatively large heat capacity for absorbing heat dissipated from the contact area. In the case of a bipolar forceps known from DE 10 2008 022 889 A1, a channel leading to the contact area of the electrodes is worked into the distal ends of the limbs, consisting of stainless steel, of the forceps, which channel is filled with silver to form a heat conduction channel for dissipating the heat from the contact areas. In these known bipolar forceps, the formation of the heat dissipation is connected with additional work steps during the production of the forceps.

### BRIEF SUMMARY OF THE INVENTION

The invention is based on the object of simplifying the production of a bipolar forceps as per the preamble of claim 1.

According to the invention, this object is achieved by a bipolar forceps with the features of patent claim 1. According to the invention, such a forceps is produced by a method as per patent claim 9.

Advantageous embodiments of the invention are specified in the dependent claims.

In the case of the bipolar forceps according to the invention, the two limbs of the forceps are each produced from a bimetal material, which consists of a first layer of an elasti-

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cally resilient metal and a second layer made of a metal with high electrical and thermal conductivity. The bimetal material is produced in a fashion known per se by placing a strip made of the elastically resilient metal and a strip made of the metal with the high conductivity flat on top of one another and connecting them integrally. The integral connection is usually brought about by cold welding under pressure, more particularly by rolling. The limbs of the forceps are made by deformation from the bimetal strip produced thus. To this end, the limbs of the forceps are stamped out of the bimetal strip, preferably available in the form of a large-area metal strip, and deformed under pressure. This affords the possibility of producing the blanks of the limbs of the forceps from the bimetal strip in a single work step by stamping and compression processing by means of a press.

The first layer made of the elastically resilient metal in the process forms the outer side of the limbs, while the second layer made of the metal with the high electrical and thermal conductivity forms the inner sides of the limbs facing one another. Here, the first layer provides the limbs of the forceps with the mechanical rigidity and the resilient properties for opening and closing the forceps. The electrodes are formed at the distal end of the limbs from the metal of the second layer. As a result of its areal extent, the second layer has a high heat capacity, with the high thermal conductivity ensuring rapid dissipation of the heat from the electrodes into the volume of the second layer.

The first layer, which forms the outer side of the limbs of the forceps, preferably consists of stainless steel. Silver or a silver alloy is preferably selected as biocompatible metal with high thermal and electrical conductivity for the second layer.

The second layer should preferably at least extend over half the length of the limb at the distal end of the limb in order to provide a sufficient volume of this layer and hence sufficient heat capacity for absorbing the dissipated heat. However, the second layer preferably extends over the entire inner surface of the limbs. A first advantage of this is the particularly high thermal capacity, and it also simplifies the production in particular because the blanks of the limbs can be stamped out of a bimetal strip with two layers throughout.

### BRIEF DESCRIPTION OF THE DRAWINGS

In the following text, the invention will be explained in more detail on the basis of an exemplary embodiment illustrated in the drawing, in which:

FIG. 1 shows a bimetal strip as basic material for producing the limbs of a bipolar forceps,

FIG. 2 shows a section through the bimetal strip,

FIG. 3 shows a blank of a limb of the forceps formed from the bimetal strip, in a view from the outer side and from the inner side,

FIG. 4 shows a side view of the limb,

FIG. 5 shows an enlarged view of the distal end of the limb,

FIG. 6 shows a perspective view of the bipolar forceps and

FIG. 7 shows a side view of this forceps.

In the drawing, a bipolar forceps for RF coagulation is, as an example, illustrated in an embodiment with straight limbs. Forceps with other limb shapes, e.g. curved limbs, are likewise conventional. Since the invention relates to the structure of the limbs of the forceps and not to the shape thereof, all shapes of forceps that have the structure explained below fall within the scope of the invention.

### DETAILED DESCRIPTION OF THE INVENTION

In order to produce the forceps, a bimetal strip 10 is firstly produced as basic material. To this end, a strip 12 of a sheet

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made of an elastically resilient material and a strip **14** of a sheet made of a biocompatible metal with high electrical and thermal conductivity are placed flat on top of one another. The strip **12** preferably consists of stainless steel. The strip **14** preferably consists of silver or a silver alloy, more particularly of AgNiO.<sub>15</sub>. The strip **12** for example has a material thickness of 1.5 mm and the strip **14** for example has a material thickness of 1 mm. The strips **12** and **14** lying flat on top of one another are rolled onto one another under pressure, or are pressed onto one another, as a result of which a non-detachable integral connection is created in the contact zone by cold welding and the bimetal strip **10** is formed.

In a press, a blank of a limb **16** of the forceps is stamped out of the bimetal strip **10** in a single work stroke of the press and deformed under pressure. Depending on the areal dimensions of the bimetal strip **10**, one or more limbs **16** can be produced in one work stroke of the press.

As shown in FIGS. **3** to **5**, the limb **16** has a first layer **18**, which forms the outer side of the limb **16** and is formed from the deformed strip **12** of e.g. stainless steel. The inner side of the limb **16** is formed by a second layer **20**, which is formed from the strip **14** of e.g. a silver alloy. In the illustrated exemplary embodiment, the first layer **18** and the second layer **20** extend with their areas substantially parallel over the entire length and width of the limb **16**.

In the longitudinal direction, the limb **16** has a proximal end region **22**, a central region **24** and a distal end region **26**. In the proximal end region **22**, the limb **16** has a reduced width and is deformed to have a low material thickness, wherein the material thickness of the outer first layer **18** and inner second layer **20** is approximately equal. The central region **24** has a greater width, with the outer first layer **18** being formed to make a serrated recessed grip **28**. The inner second layer **20** is not deformed in this region, and so the material thickness of the inner second layer **20** in conjunction with the width of the central region **24** forms a large volume with a high heat capacity.

The distal end region **26** of the limb **16** has a small width and tapers towards the distal tip of the limb. The second layer **20** is formed to be an electrode **30** in the region of the distal tip. In the region of this electrode **30**, the material thickness of the second layer **20** is enlarged, and so the electrode **30** projects over the plane of the inner side of the limb **16** with a raised contact area **32**. The second layer **20** ensures a good thermally conducting connection between the electrode **30** and the volume of the second layer **20** in the region of the recessed grip **28**, and so rapid heat dissipation is ensured from the electrode **30** to the thermal capacity of the second layer **20** in the region of the recessed grip **28**. With the exception of the raised electrode **30**, the second layer **20** forms a continuous planar surface over the entire inner side of the limb **16**.

As shown by FIGS. **6** and **7**, two limbs **16** are joined together in a mirror-symmetric fashion with inner sides facing one another in order to form the forceps. In the process, the proximal end regions **22** of the two limbs are encapsulated by molding by an insulating plastic material. This plastic material forms an electrical insulation **34** between the inner faces facing one another of the proximal end regions **22** of the two limbs **16**. Furthermore, the plastic material forms an outer collar **36**, which surrounds the proximal end regions **22** of the two limbs **16** and holds these together mechanically. The end of the limbs **16** projecting beyond the outer collar **36** in the proximal direction forms a plug **38** of a plug-in connection for an RF current supply with the first layers **18**, which are respectively exposed on the outer side. On the distal side of the outer collar **36**, the limbs **16** are coated by a plastic

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insulation that, it goes without saying, leaves at least the contact areas **32** of the electrodes **30** exposed.

During use, the forceps is connected to an RF current supply via the plug **38**. For the purposes of tissue coagulation, the tissue to be coagulated is gripped with the distal tip of the forceps such that the two limbs **16** of the forceps each touch the tissue to be coagulated with the contact areas **32** of the electrodes **30**. A radiofrequency current can now be conducted through the tissue via the electrodes **30**, as a result of which the tissue between the electrodes **30** is heated and coagulates. Heat generated at the contact areas **32** is absorbed by the electrode **30** and very rapidly dissipated from the electrode **30** to the large volume of the second layer **20** as a result of the high thermal conductivity of the second layer **20** and the relatively large cross section thereof. As a result, it is possible to prevent the contact areas **32** from being heated and tissue from sticking onto the contact areas **32** as a result thereof.

#### LIST OF REFERENCE SIGNS

**10** Bimetal strip  
**12** Stainless steel strip  
**14** Silver strip  
**16** Limb  
**18** First layer  
**20** Second layer  
**22** Proximal end region  
**24** Central region  
**26** Distal end region  
**28** Recessed grip  
**30** Electrode  
**32** Contact area  
**34** Insulation  
**36** Outer collar  
**38** Plug

The invention claimed is:

1. Bipolar forceps, more particularly for RF coagulation, with two limbs (**16**) made of an elastically resilient metal, with electrodes (**30**) arranged at the distal ends (**26**) of the limbs (**16**), the contact area (**32**) of which electrodes being formed by a biocompatible metal with high electrical and thermal conductivity, and with an electrical plug-in connector (**38**) arranged at the proximal end (**22**) of the forceps, characterized in that the limbs (**16**) each consist of a bimetal material at least in the distal end regions (**26**) thereof, which bimetal material further constitutes, on the outer sides of the limbs (**16**) facing away from one another, a first layer (**18**), which is formed by the elastically resilient metal, and, on the inner sides of the limbs (**16**) facing one another, a second layer (**20**), which is made of the metal with the high electrical and thermal conductivity, and in that the electrodes (**30**) are each formed from the second layer (**20**).

2. Forceps according to claim 1, characterized in that the first layer (**18**) consists of stainless steel.

3. Forceps according to claim 1, characterized in that the second layer (**20**) consists of silver or a silver alloy.

4. Forceps according to claim 2, characterized in that the second layer (**20**) consists of silver or a silver alloy.

5. Forceps according to claim 3 or 4, characterized in that the second layer (**20**) consists of AgNiO.<sub>15</sub>.

6. Forceps according to claim 1, 2 or 3, characterized in that the first layer (**18**) and the second layer (**20**) are interconnected by rolling or pressing.

7. Forceps according to claim 1, 2 or 3, characterized in that the second layer (**20**) at least extends over the distal half of the longitudinal extent of the limbs (**16**).

8. Forceps according to claim 1, 2 or 3, characterized in that the second layer (20) extends over the entire surface of the inner side of the limbs (16).

9. Forceps according to claim 1, 2 or 3, characterized in that the limbs have an insulating coating, which leaves at least the contact area (32) of the electrodes (30) exposed.

10. Forceps according to claim 1, characterized in that a major portion of the distal end regions (26) of the limbs (16) are constructed of the bimetal material in which the first layer (18) forms the outer sides of the limbs (16) and the second layer (20) forms the inner sides of the limbs (16).

\* \* \* \* \*

UNITED STATES PATENT AND TRADEMARK OFFICE  
**CERTIFICATE OF CORRECTION**

PATENT NO. : 9,242,351 B2  
APPLICATION NO. : 13/171575  
DATED : January 26, 2016  
INVENTOR(S) : Thomas Butsch

Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

On the title page

Item 57 in the Abstract, Line 5, please change “sliver” to --silver--.

Signed and Sealed this  
Twenty-ninth Day of November, 2016

A handwritten signature in black ink, reading "Michelle K. Lee". The signature is written in a cursive style with a large, stylized "M" and "L".

Michelle K. Lee  
*Director of the United States Patent and Trademark Office*